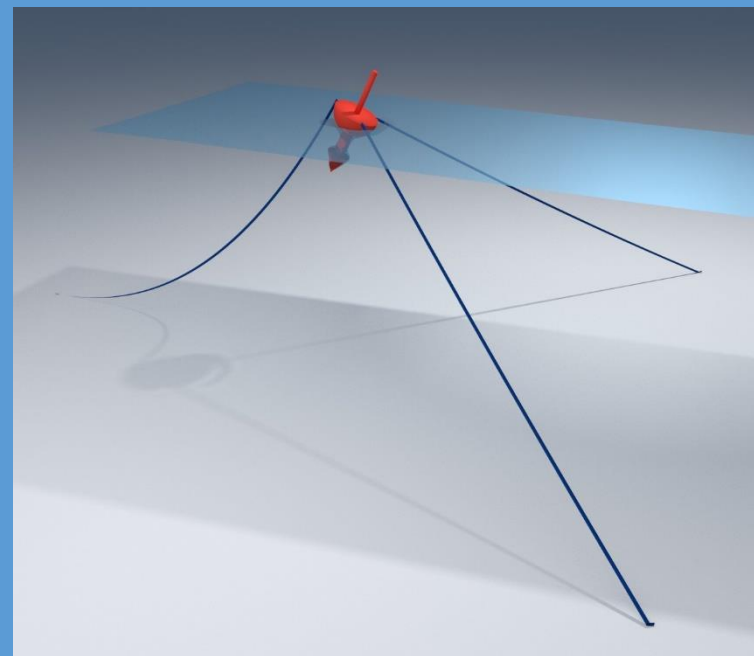
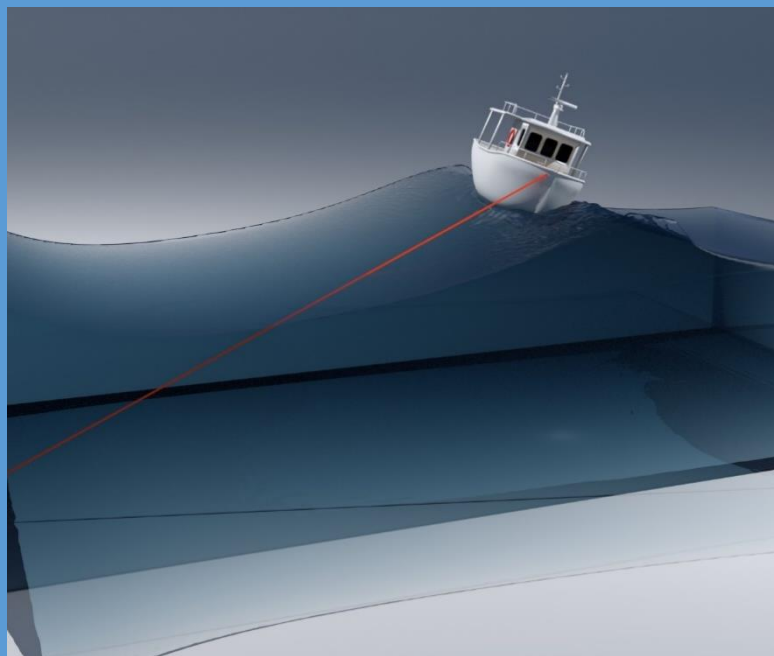


# Mooring implementation in SPH models



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1. Introduction

2. Floatings & moorings

3. Conclusions

1.1 What is a mooring?

1.2 Why is important to solve moorings?







All the objects are floating in the water and moored, thus a proper formulation is needed and must be validated.

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  2. Floatings & moorings
  3. Run-off on real terrains
  4. Conclusions & future work
- 2.1 Fluid driven objects
  - 2.2 Moored lines
    - 2.2.1 Static approach
    - 2.2.2 Mooring classification
    - 2.2.3 Model validation
  - 2.3 Application cases

Each particle  $k$  (FB) experiences a force per unit mass given by  $\mathbf{f}_k = \sum_{a \in WPs} \mathbf{f}_{ka}$

Where  $\mathbf{f}_{ka}$  is the force per unit mass by the fluid  $a$  on particle  $k$ ,

$$m_k \mathbf{f}_{ka} = -m_a \mathbf{f}_{ak}$$

Newton's equations for **rigid body dynamics**:

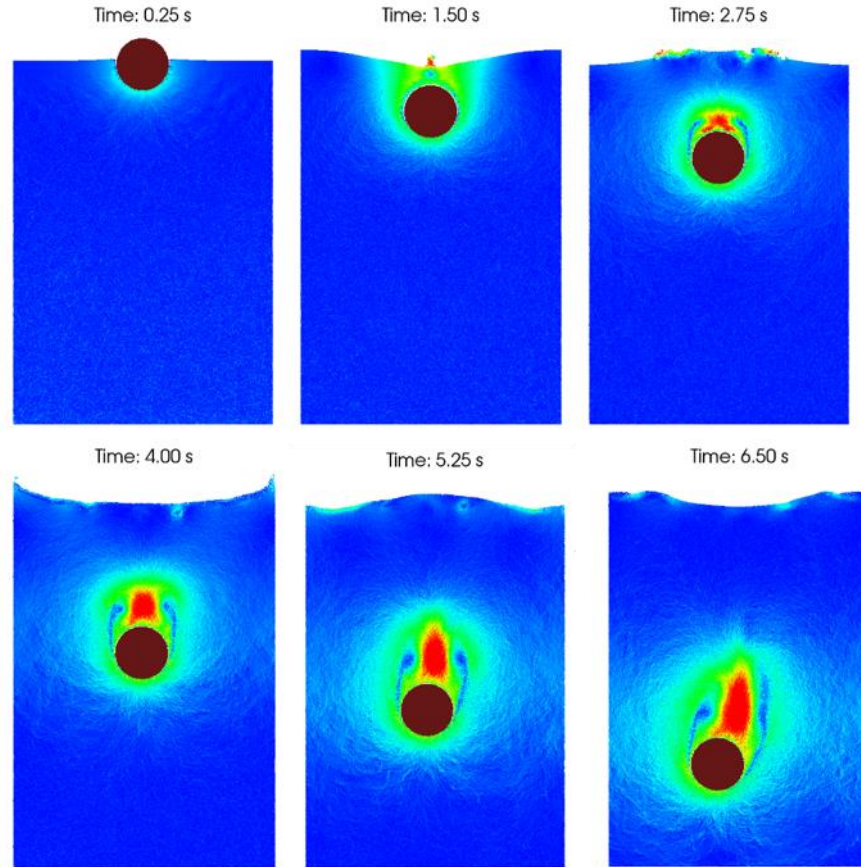
$$M \frac{d\mathbf{V}}{dt} = \sum_{k \in BPs} m_k \mathbf{f}_k$$

$$I \frac{d\boldsymbol{\Omega}}{dt} = \sum_{k \in BPs} m_k (\mathbf{r}_k - \mathbf{R}_0) \times \mathbf{f}_k$$

$$\mathbf{u}_k = \mathbf{V} + \boldsymbol{\Omega} \times (\mathbf{r}_k - \mathbf{R}_0)$$

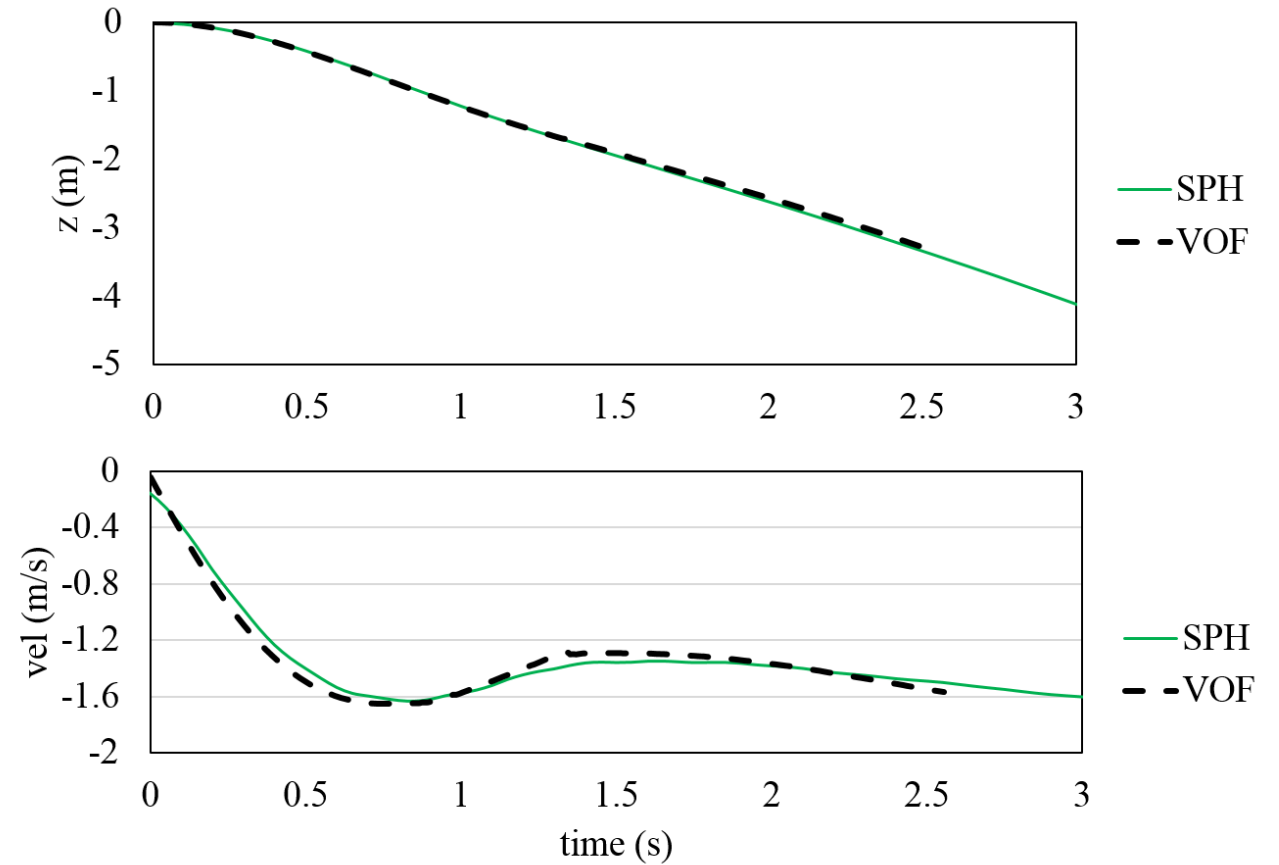
The movement of FB is derived by considering its interaction with fluid particles and using these forces to drive its motion

## Validation for floating objects



$$\rho_{object} = 1,200 \text{ kg} \cdot \text{m}^{-3}$$

Comparison of **numerical data** and **DualSPHysics** results for **displacement** and **velocity** of the sinking cylinder.



Fekken (2004) & Canelas et al. (2015)





Catenary function  $y = \xi \cosh\left(\frac{x}{\xi}\right)$

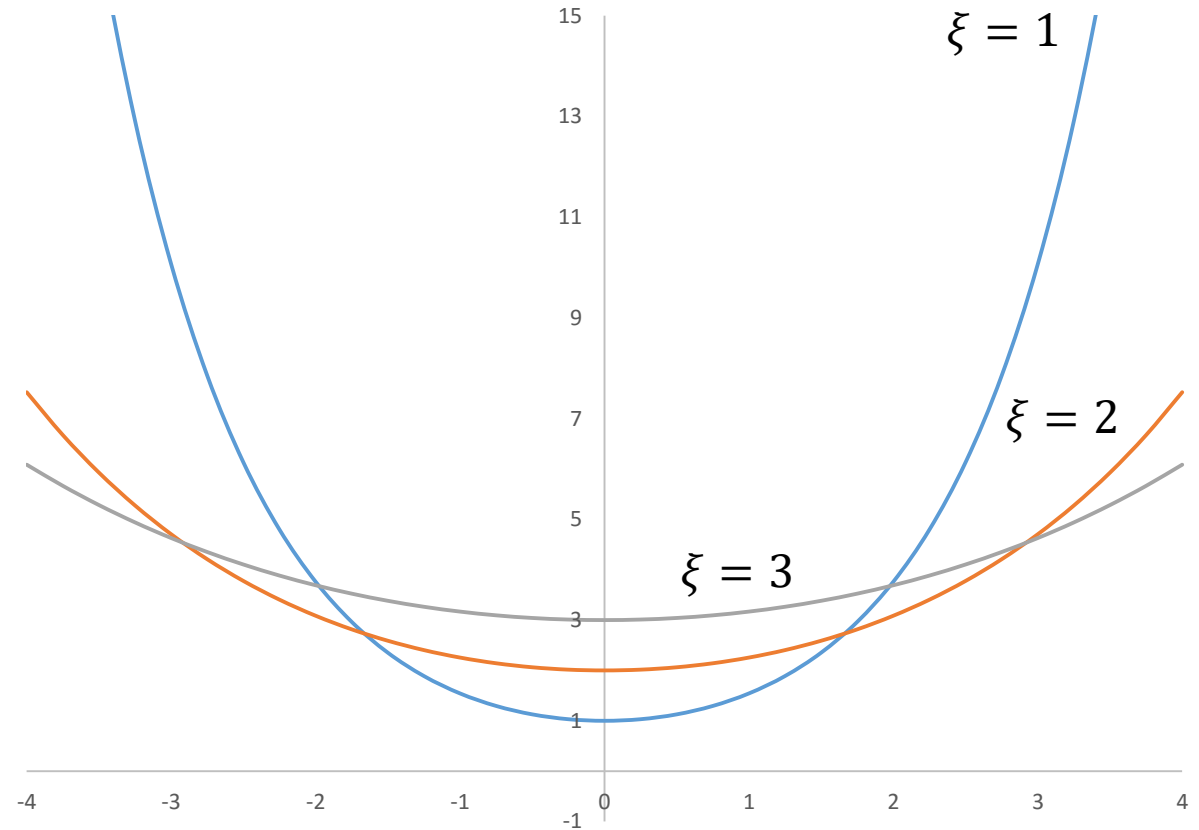
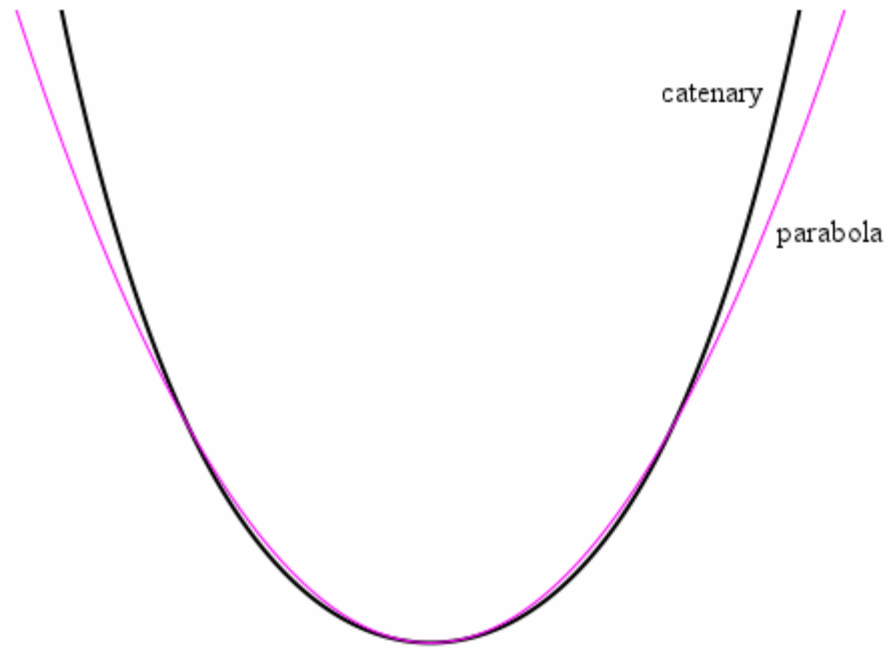
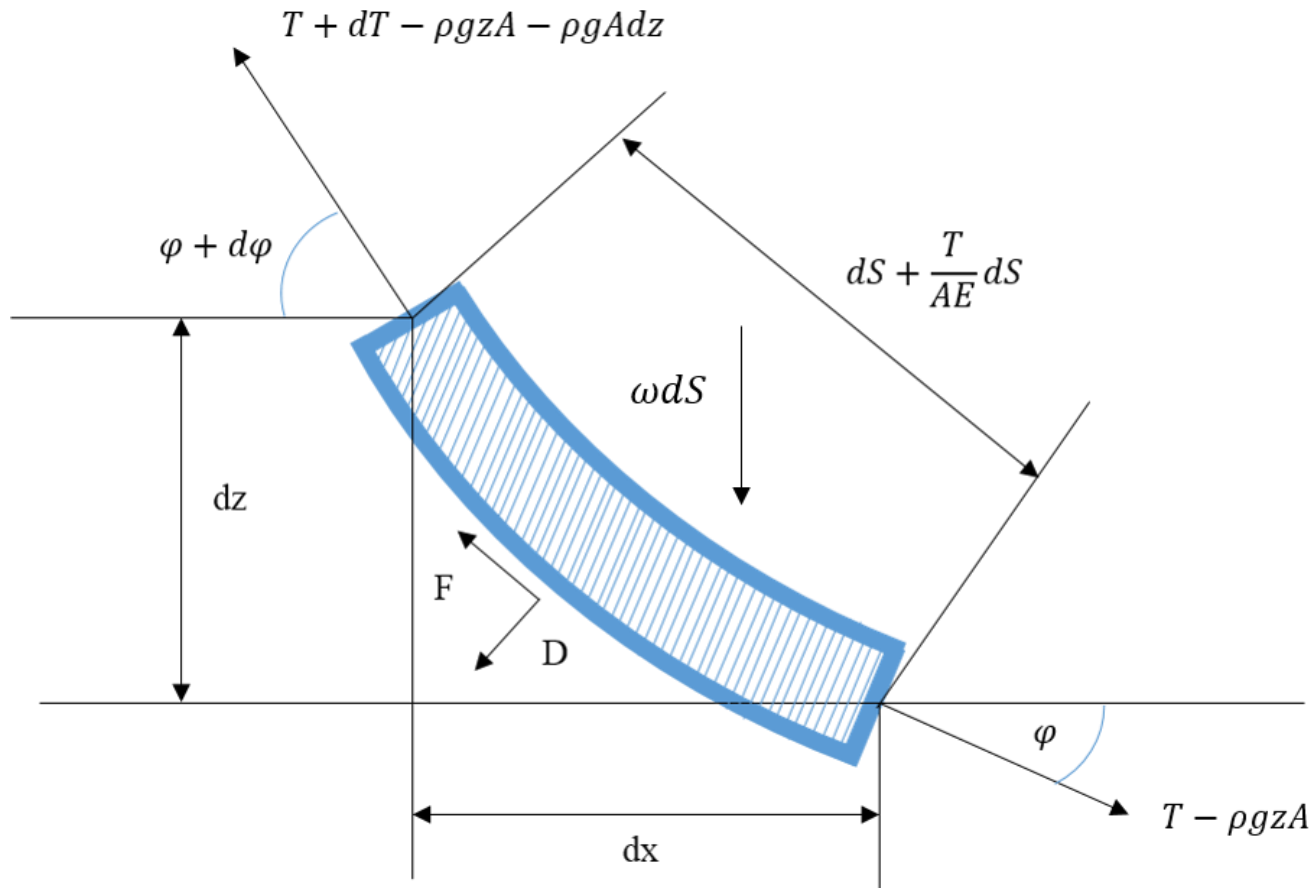


Diagram of the different forces acting on an element of a mooring line



$T$  is the line **tension**.

$A$  is the **cross-section** area of the line.

$E$  represents the **elasticity modulus**.

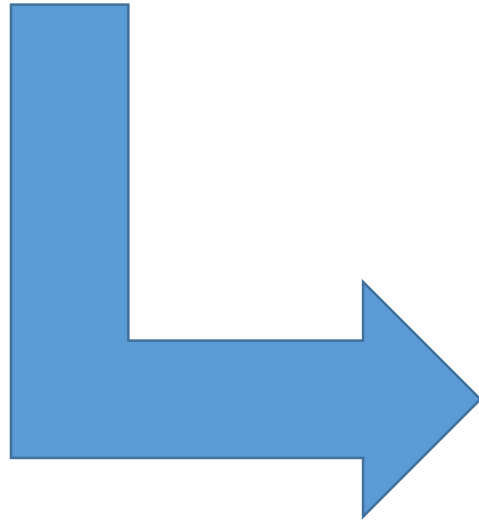
$F$  and  $D$  correspond to the **mean hydrodynamic forces** both normal and tangential direction respectively.

$\omega$  is the **submerged weight** per unit length.

$$dT - \rho g A dz = \left[ \omega \sin \phi - F \left( 1 + T / (AE) \right) \right] ds$$

$$T d\phi - \rho g A d\phi = \left[ \omega \cos \phi + D \left( 1 + T / (AE) \right) \right] ds$$

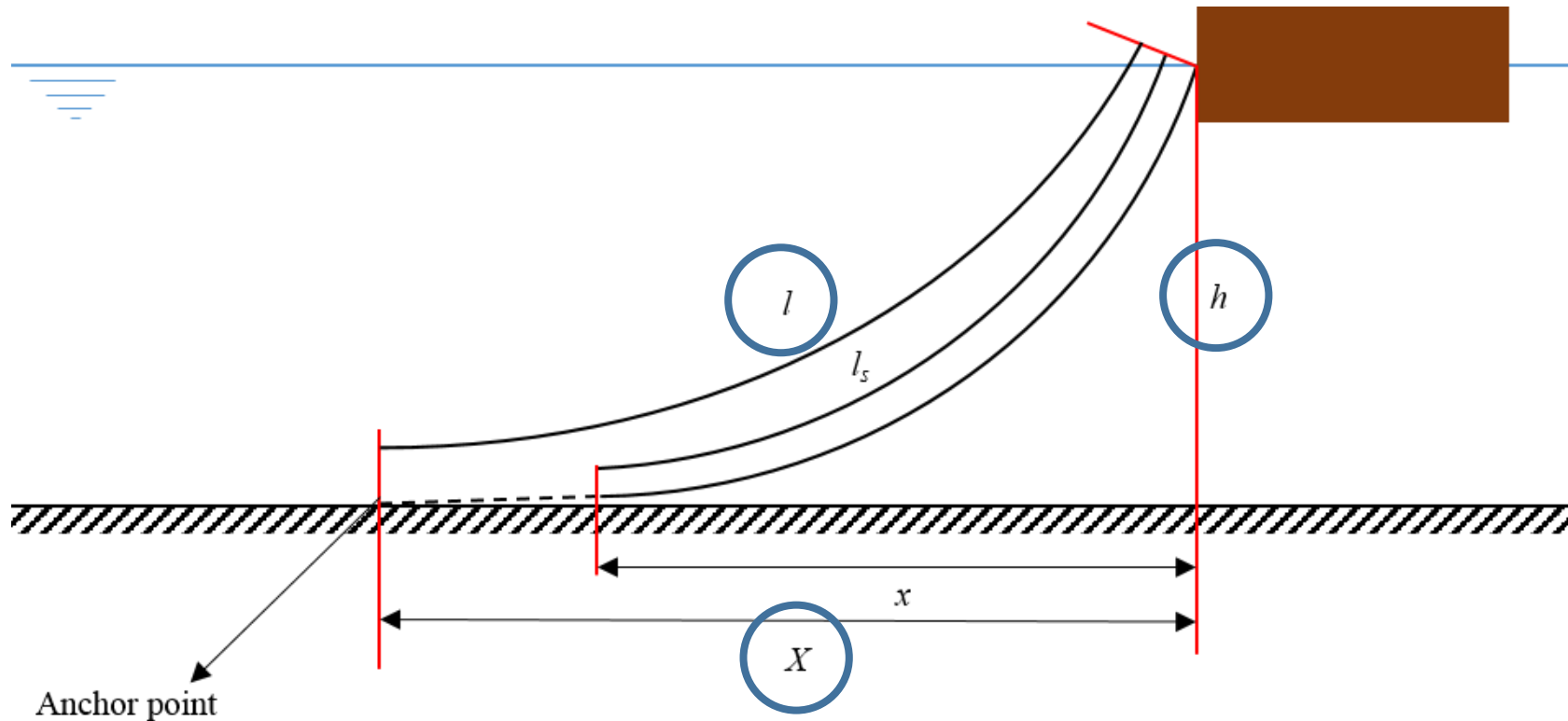
Faltinsen (1993)



The **tension exerted by a mooring** on a **floating body** can be expressed as:

$$T = T_H + \omega h + (\omega + \rho g A)z$$

Parameters that define a mooring line.

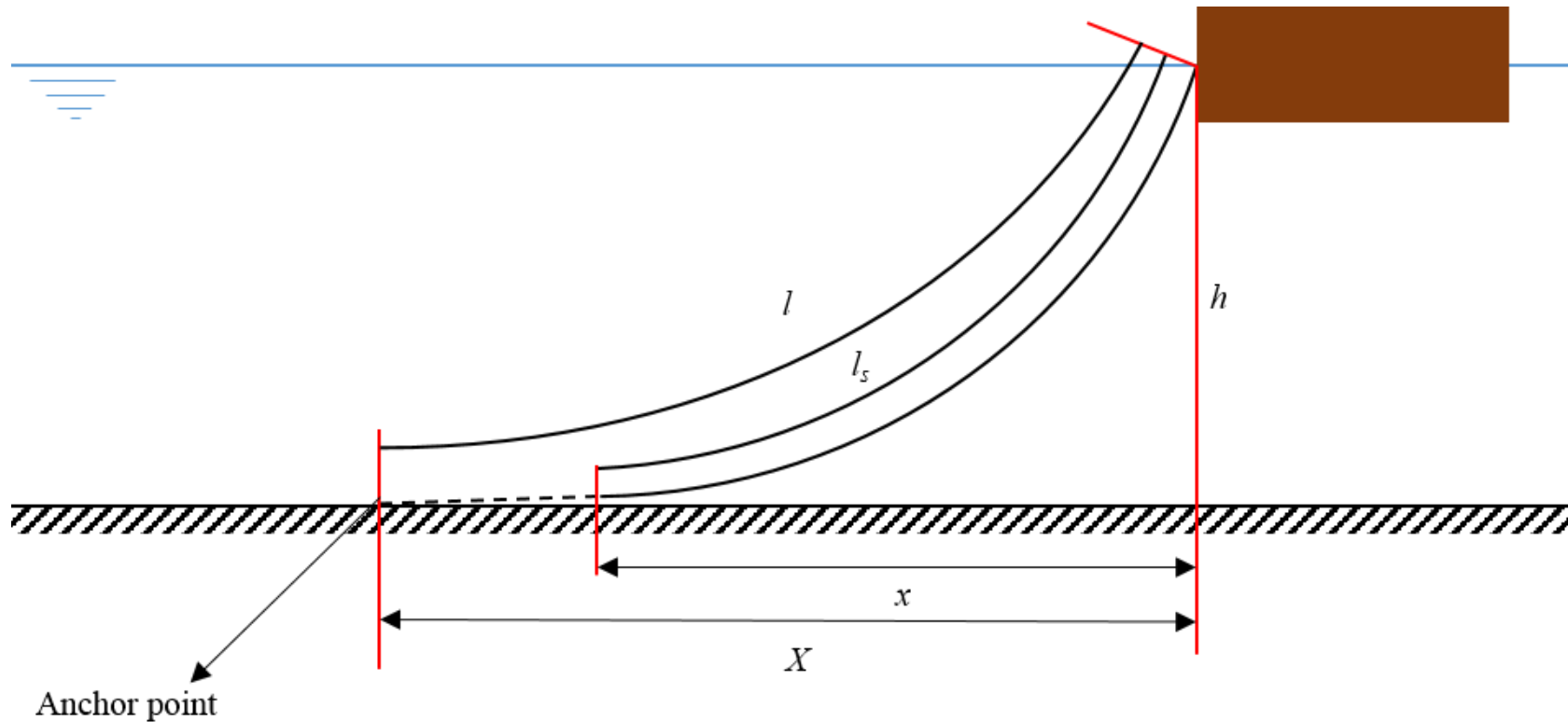




Parameters that define a mooring line.

$$a = T_H / \omega$$

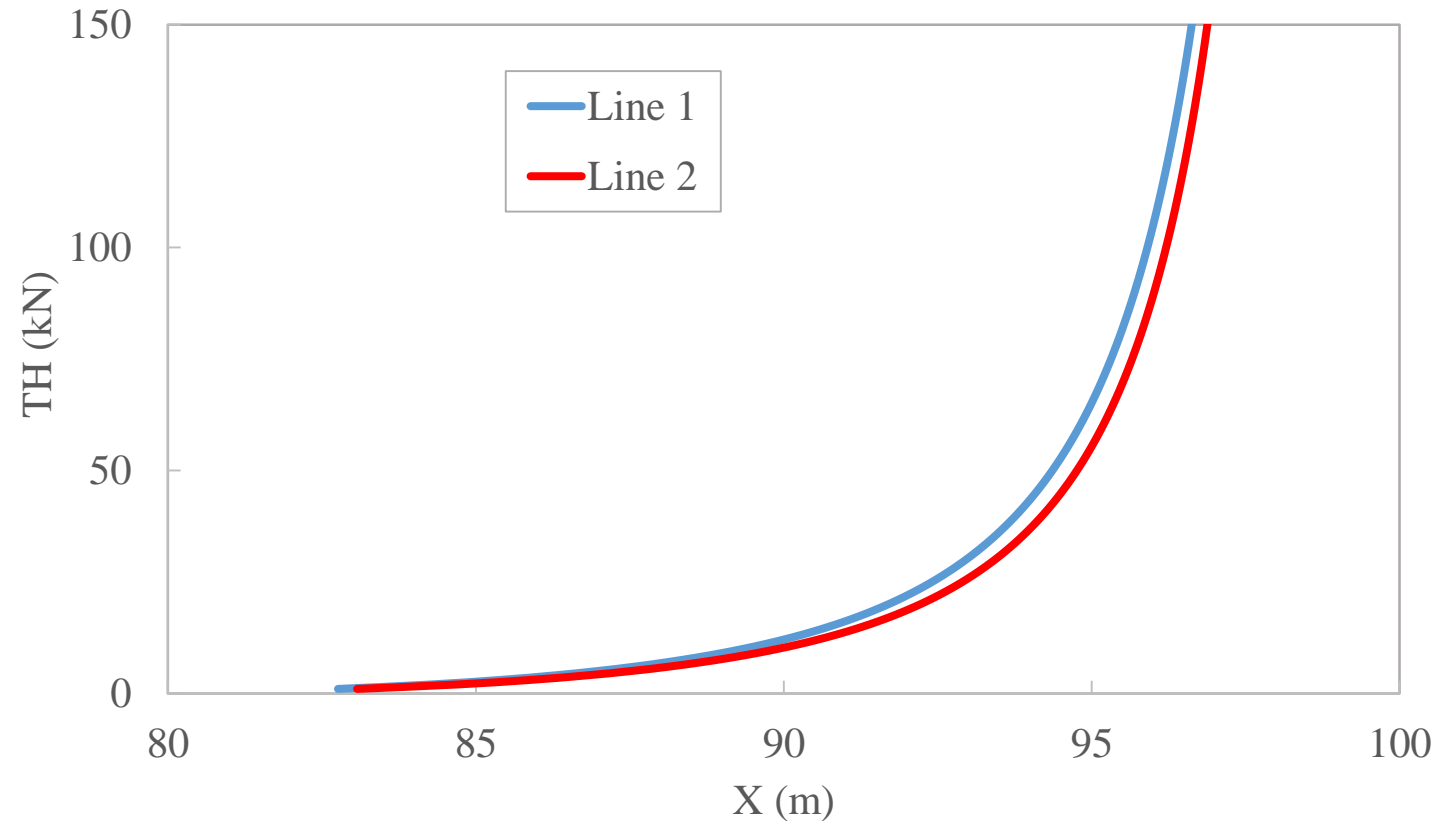
$$X = l - h \left( 1 + 2 \frac{a}{h} \right)^{\frac{1}{2}} + a \cosh^{-1} \left( 1 + \frac{h}{a} \right)$$



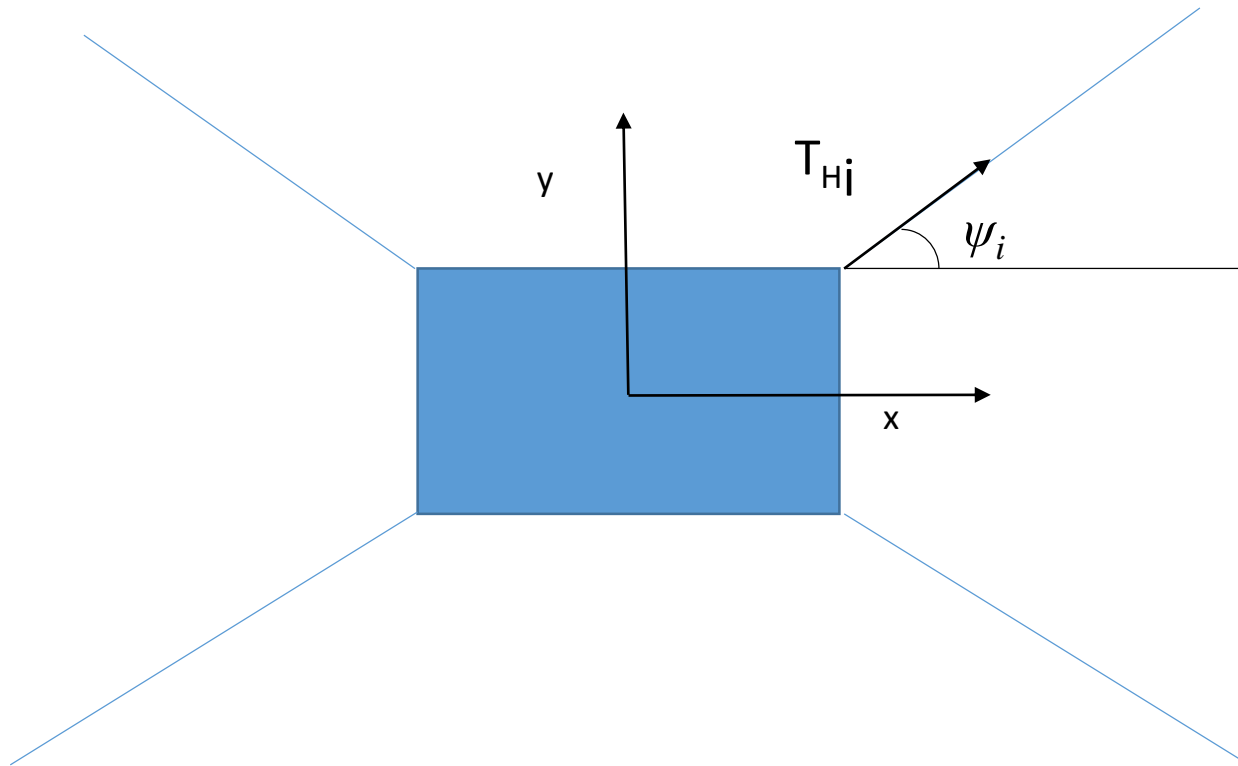
$$a = T_H / \omega$$

$$X = l - h \left( 1 + 2 \frac{a}{h} \right)^{\frac{1}{2}} + a \cosh^{-1} \left( 1 + \frac{h}{a} \right)$$

- Line 1,  $\omega=850 \text{ N}\cdot\text{m}^{-1}$ ,  $h=20 \text{ m}$  and  $l=100 \text{ m}$ .
- Line 2,  $\omega=1000 \text{ N}\cdot\text{m}^{-1}$ ,  $h=20 \text{ m}$  and  $l=100 \text{ m}$ .



Spread mooring approach:

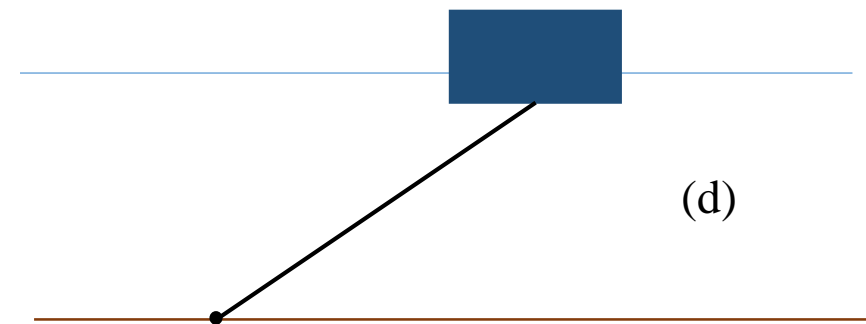
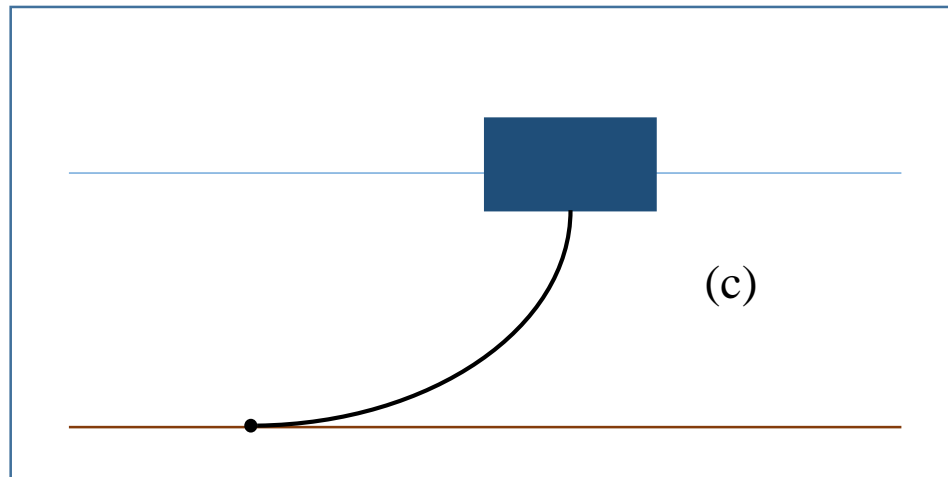
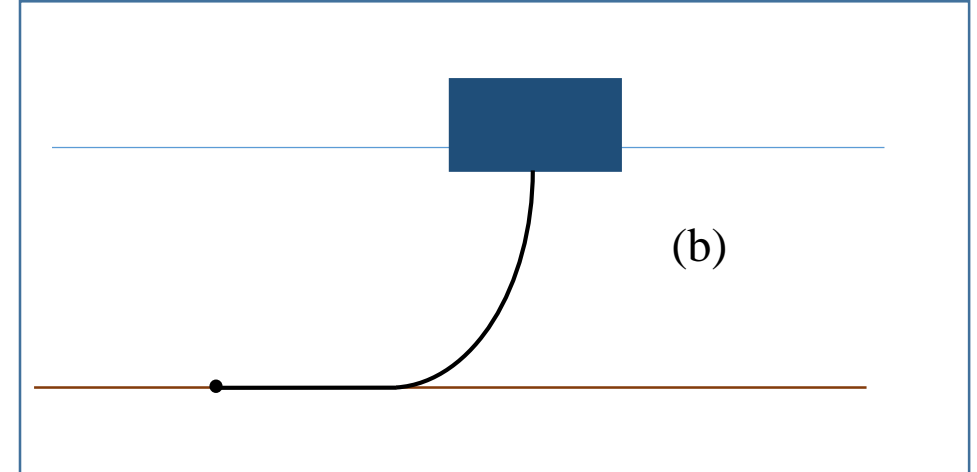
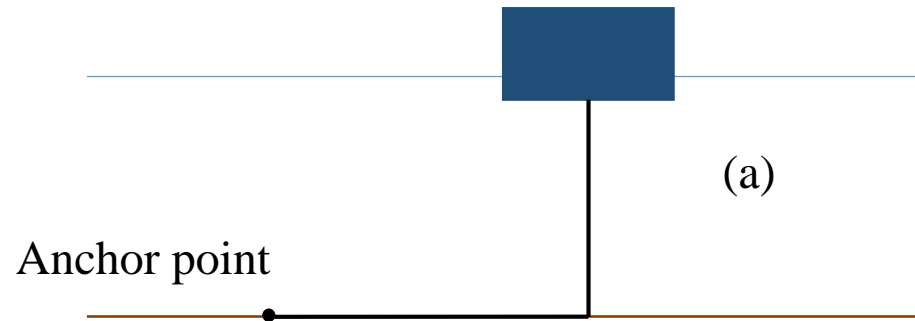


The equations shown before can be generalized for a multiple line problem with the proper implementation.

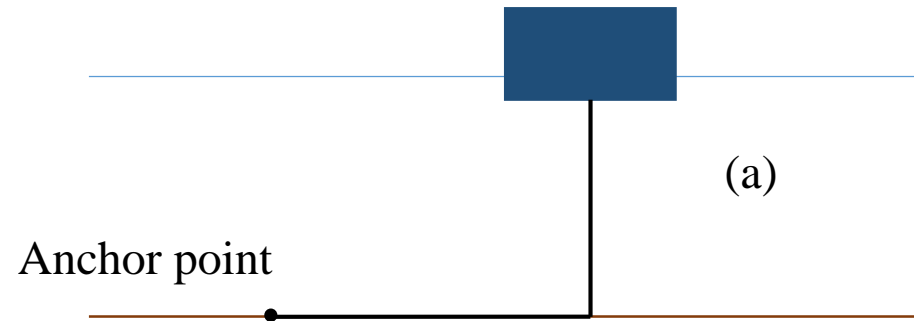
$$F_x = T_{Hi} \cos \Psi_i$$

$$F_y = T_{Hi} \sin \Psi_i$$

Normal conditions are already covered but there are two different states that are not solved yet



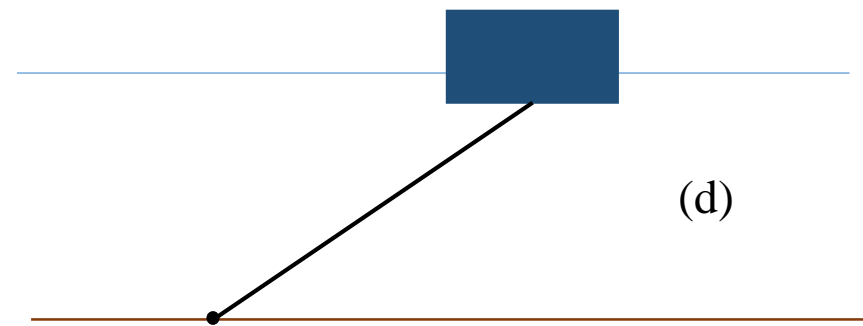
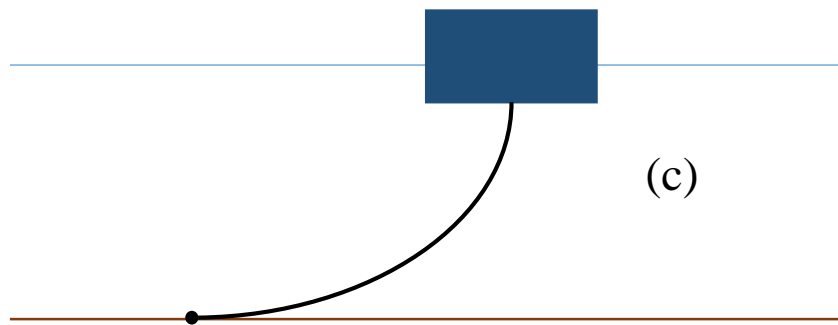
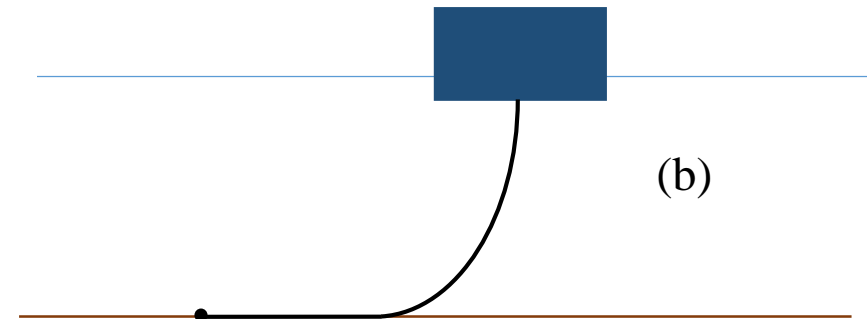
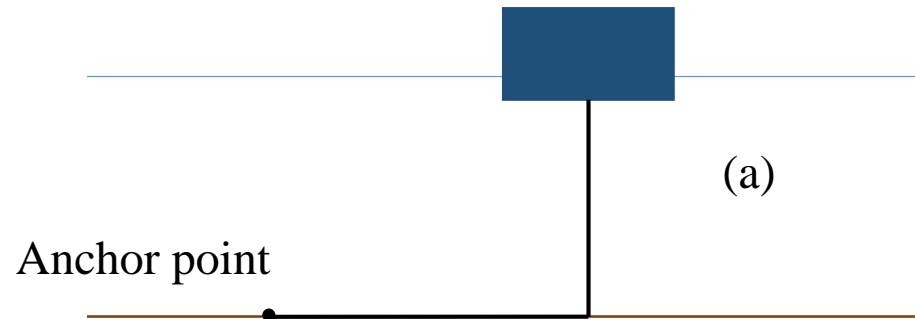
Normal conditions are already covered but there are two different states that are not solved yet



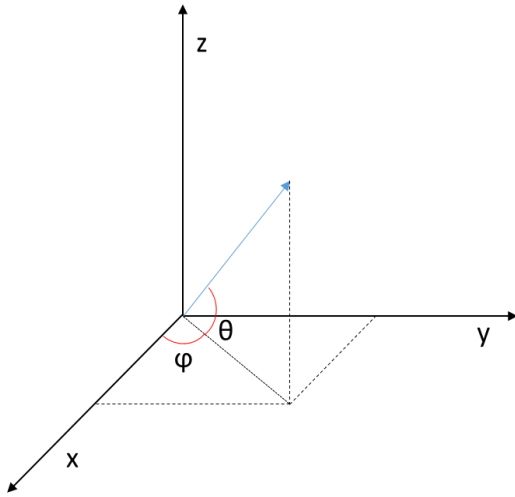
$$T_z \cong \omega h g$$



Normal conditions are already covered but there are two different states that are not solved yet

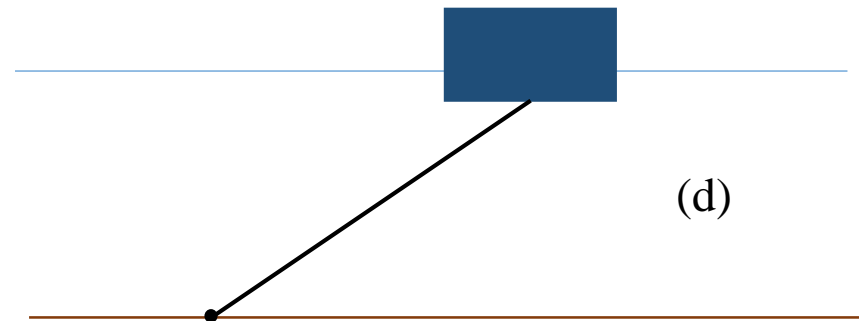


Normal conditions are already covered but there are two different states that are not solved yet



$$\begin{aligned}
 \mathbf{F}_T &= \mathbf{F}_1 + \mathbf{F}_2 + \mathbf{F}_3 + \mathbf{F}_4 \dots \\
 F_{Tx} &= F_T \cdot \cos \theta_T \cdot \cos \varphi_T \\
 F_{Ty} &= F_T \cdot \cos \theta_T \cdot \sin \varphi_T \\
 F_{Tz} &= F_T \cdot \sin \theta_T
 \end{aligned}$$

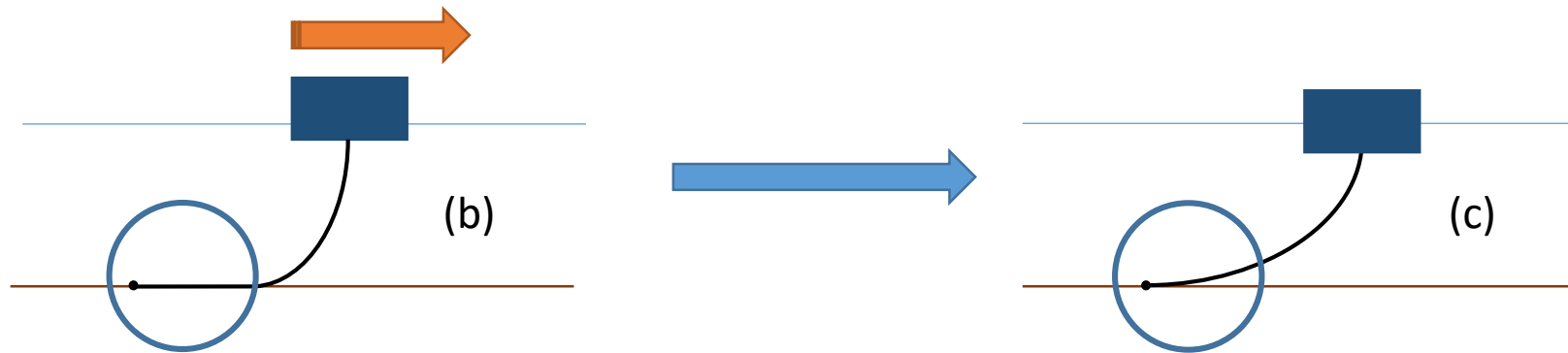
$$\text{Force for } i \text{ mooring} \left\{ \begin{aligned}
 F_{ix} &= \frac{F_{Tx} \cdot \cos \varphi_i}{\sum_j^n \cos \varphi_j} \\
 F_{iy} &= \frac{F_{Ty} \cdot \sin \varphi_i}{\sum_j^n \sin \varphi_j} \\
 F_{iz} &= \frac{F_{Tz} \cdot \sin \theta_i}{\sum_j^n \sin \theta_j}
 \end{aligned} \right.$$



(d)

## One line validation I

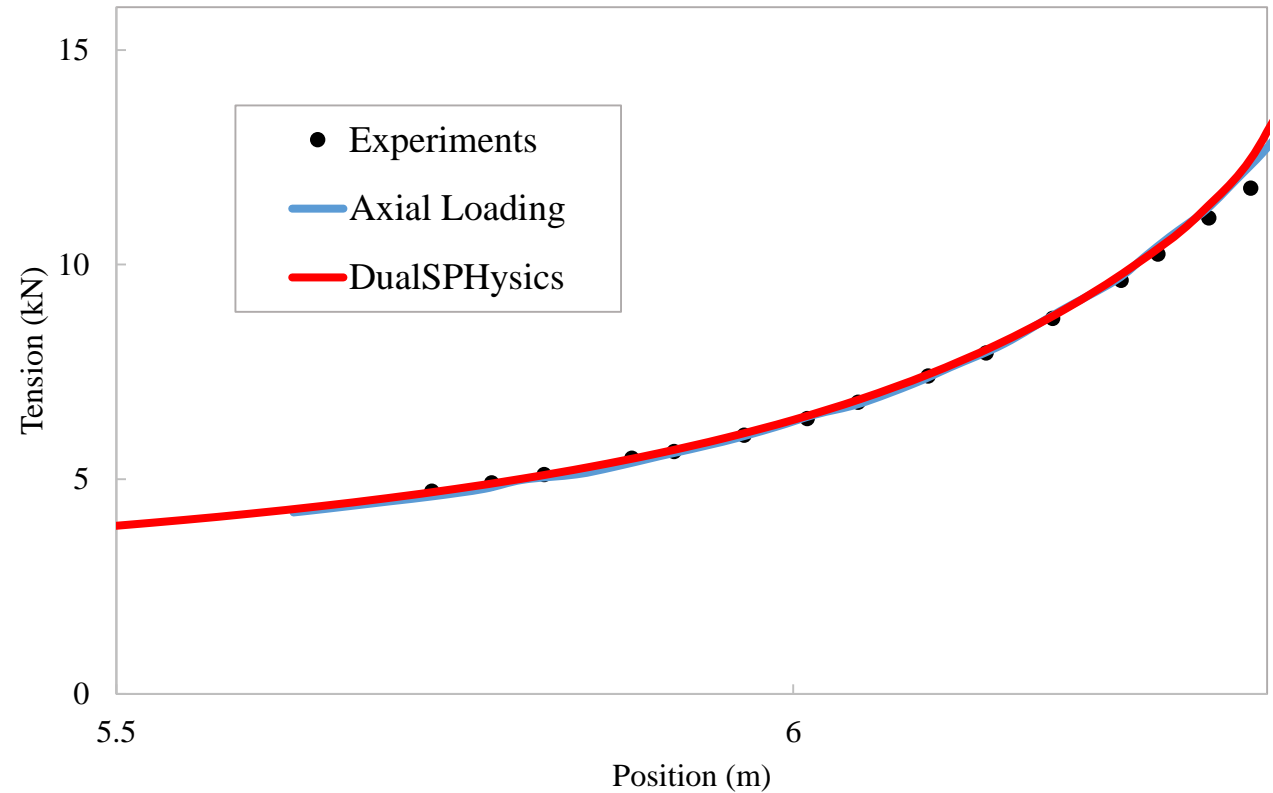
Johanning (2007), Laboratory dimensions.



## One line validation I

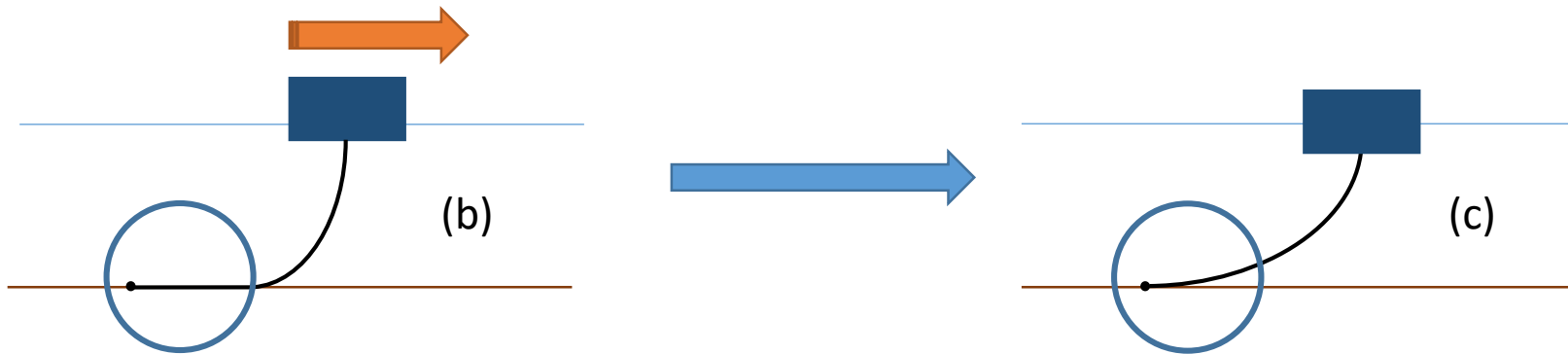
Johanning (2007), Laboratory dimensions.

Parameter	Value
h	2.651 m
$\omega$	1.036 N·m <sup>-1</sup>
l	6.98 m
Minimum extension	5.735 m
Maximum extension	6.367 m



## One line validation II

Johanning (2006), Real dimensions.

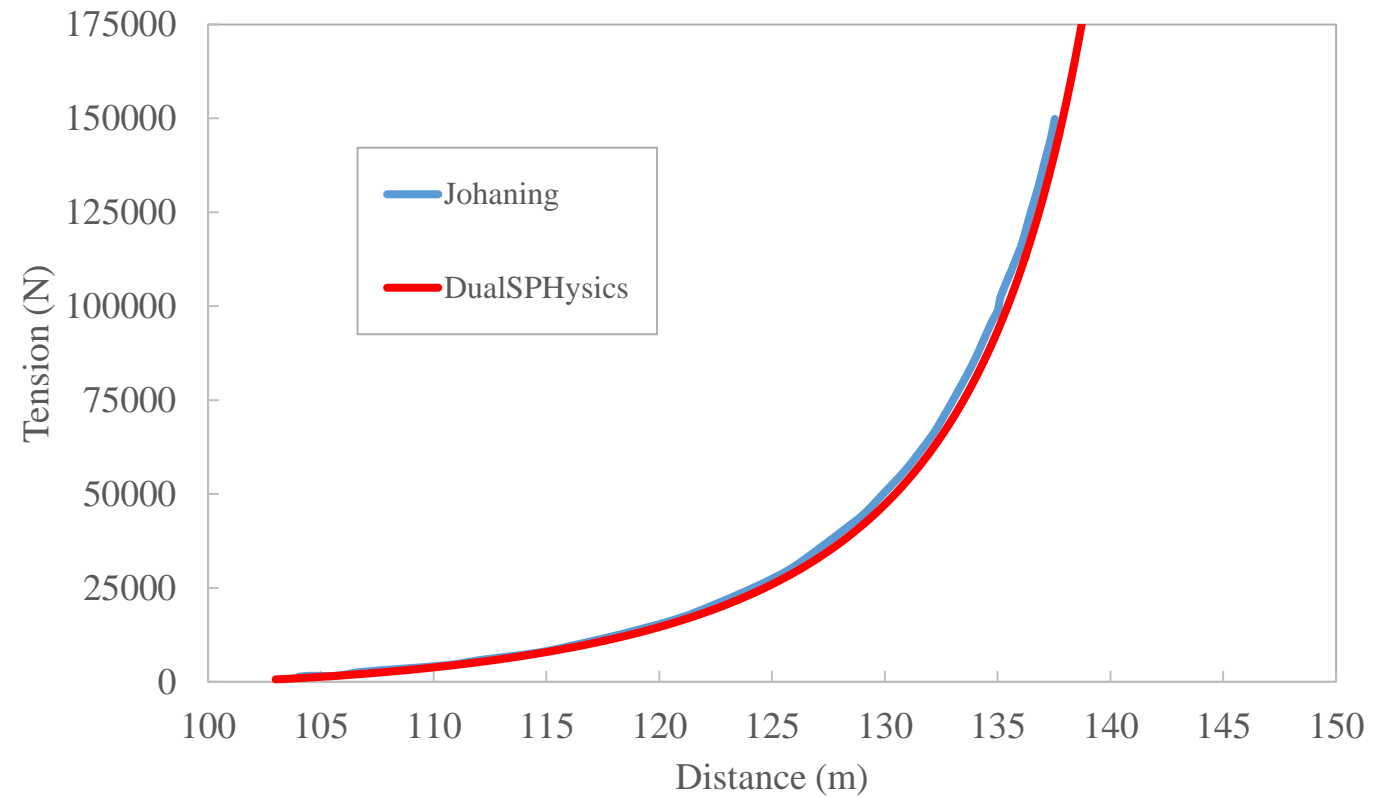




## One line validation II

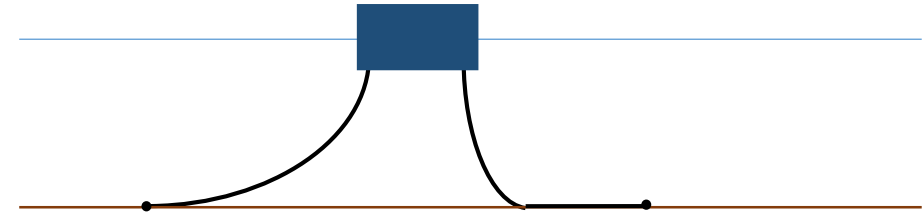
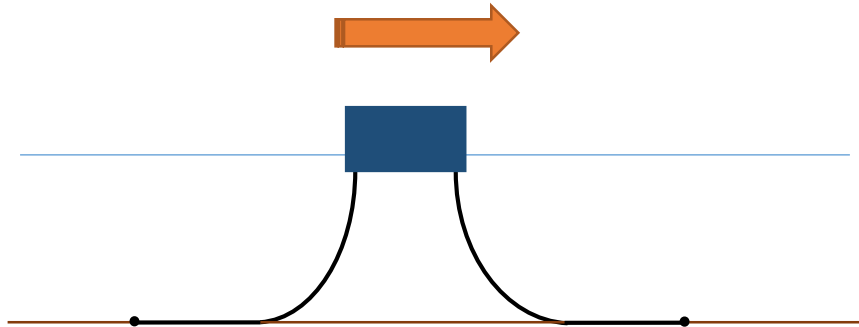
Johanning (2006), Real dimensions.

Parameter	Value
h	50 m
$\omega$	918.75 N·m <sup>-1</sup>
l	150 m
Minimum extension	102 m
Maximum extension	140 m



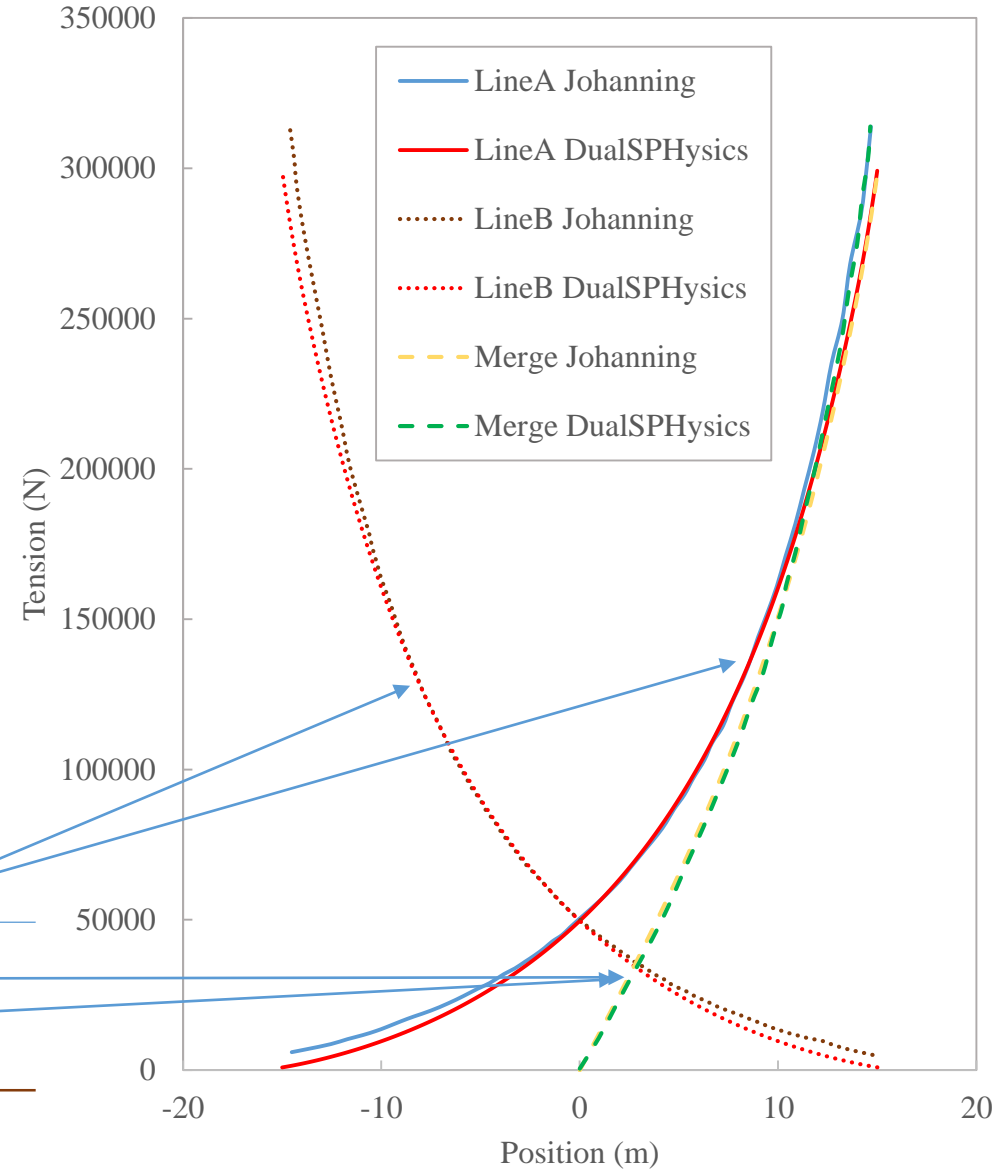
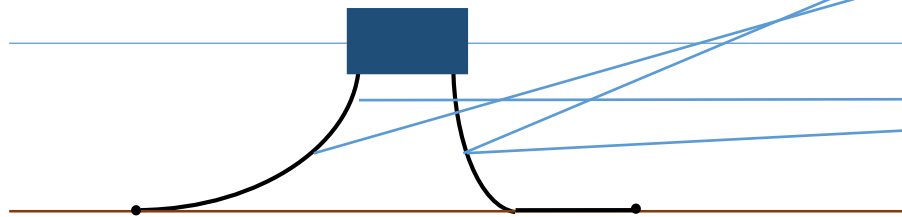
## Multiple line validation

Johanning (2006),  
Real dimensions.



## Multiple line validation

Parameter	Value
h	50 m
$T_{H0}$	50 kN
l	75 m
Minimum extension from resting point	-15 m
Maximum extension from resting point	15 m



A 3D simulation of a white boat floating in a dark blue liquid within a transparent rectangular tank. A red line originates from the boat's hull and extends to the left edge of the frame. A white rectangular box with a blue border is overlaid on the red line, containing the text "VIDEO LINK".

[VIDEO LINK](#)



[VIDEO LINK](#)

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## -Moorings & Floating bodies

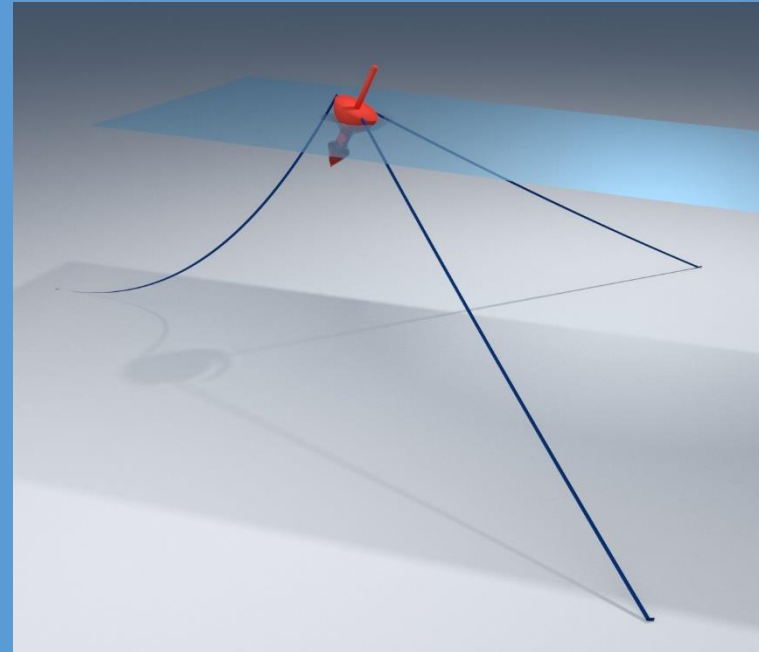
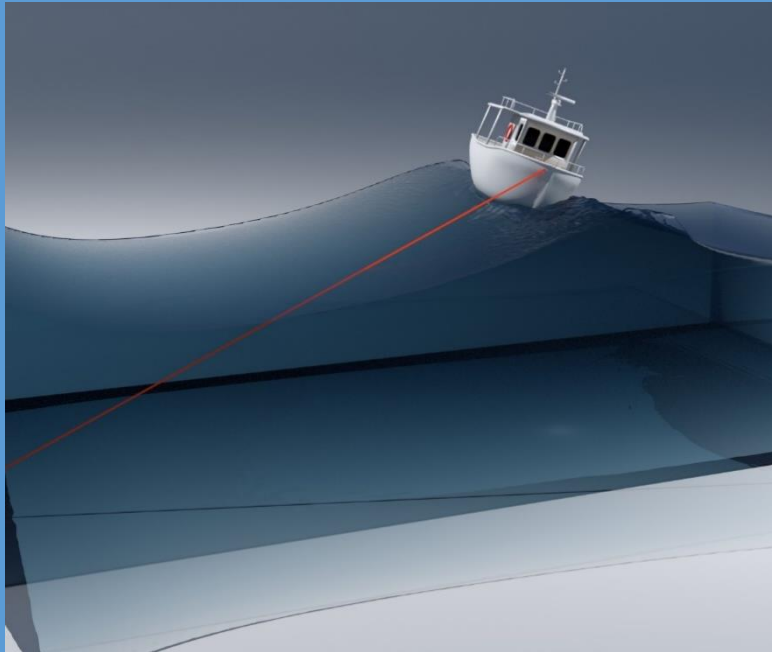
The functionalities necessary to simulate moorings were implemented in DualSPHysics. The **new implementation** is able to **solve** properly both **chain forces** and the effect moorings in the floating bodies.

The **buoyancy** of the floating bodies was **validated** against **numerical data** from VOF showing a really good agreement.

The implementation of **moorings** was **validated** against **experimental** data and compared with other **numerical models**. This validation provided really good agreement with both numerical and experimental data at various scales.

Two application **examples** were presented, the first one is a **boat** under the action of side waves and only **one moored line**. The second application consisted of a **wind-turbine base** with **three moorings** under the effect of extreme waves.

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